# Side Note: Perturbation scheme on SO(3) Rotation

Reference: State estimation for robotics by Prof. Barfoot [1]

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## Preliminary

For a more thorough treatment on Lie theory for state estimation in robotics, one may refer to:

- Barfoot's book: State Estimation For Robotics
- Chirikjian's book: Stochastic models, information theory, and Lie groups (Volume  $1 \& 2$ )
- Sola et al., (2018) A micro Lie theory for state estimation in robotics

### 1 Perturbation Applied to a Rotation on  $SO(3)$

For a rotation in 3D, perturbations can be applied either on the Lie Algebra (i.e., the tangential space) or directly on the Special Orthogonal Group  $SO(3)$  (i.e., on the manifold).

A more general discussion on the perturbation options is presented in Section 7.3.1 in [1]. Referring to [1], there are different perturbation options, which are left, middle and right perturbations. In this document, we will discuss the right and middle perturbations.

### 1.1 Perturbation on Lie Group (Right Perturbation)

For perturbation applied directly on the  $SO(3)$  manifold, we let subscript a denote the original rotation and subscript b denote the perturbed rotation. We let  $\exp(\phi_m^{\wedge})$  be a right perturbation applied to rotation matrix  $\mathbf{R}_a$ , and we have

$$
\exp\left(\boldsymbol{\theta}_{b}^{\wedge}\right) = \mathbf{R}_{b} = \mathbf{R}_{a} \exp\left(\boldsymbol{\phi}_{m}^{\wedge}\right) = \exp\left(\boldsymbol{\theta}_{a}^{\wedge}\right) \exp\left(\boldsymbol{\phi}_{m}^{\wedge}\right), \qquad \boldsymbol{\theta}_{b}, \boldsymbol{\theta}_{a}, \boldsymbol{\phi}_{m} \in \mathbb{R}^{3}, \tag{1}
$$

where  $\exp(\cdot)$  is the matrix exponential map;  $(\cdot)^\wedge$  is the skewness operator that returns the corresponding skew-symmetric matrix of a vector; and  $\theta_a$  is the corresponding angle-axis representation of the rotation matrix  $\mathbf{R}_a$ .

If we want to recover the angle-axis vector,  $\theta_b$  (i.e., the tangential vector in the tangential space), of  $\mathbf{R}_b$ , we use the matrix logarithm map as

$$
\theta_b = \ln \left( \exp \left( \theta_a^{\wedge} \right) \exp \left( \phi_m^{\wedge} \right) \right)^{\vee}
$$
  
 
$$
\approx \theta_a + J_r(\theta_a)^{-1} \phi_m,
$$
 (2)

where  $J_r(\cdot)$  is the right jacobian of  $SO(3)$  given as (see [1, Section 7.1] and [2]):

$$
J_r(\psi) = \frac{\sin \psi}{\psi} I_{3 \times 3} + (1 - \frac{\sin \psi}{\psi}) a a^T - \frac{1 - \cos \psi}{\psi} a^{\wedge}
$$
 (3a)

$$
\equiv \mathbf{I}_{3\times 3} - \frac{1 - \cos \psi}{\psi^2} \, \psi^\wedge + \frac{\psi - \sin \psi}{\psi^3} (\psi^\wedge)^2 \tag{3b}
$$

$$
\approx \mathbf{I}_{3\times 3} - \frac{1}{2} \,\boldsymbol{\psi}^{\wedge},\tag{3c}
$$

where  $\psi = ||\psi||$  is the angle of rotation with a unit of [rad];  $\mathbf{a} = \frac{\psi}{\psi}$  $\frac{\psi}{\psi}$  is a  $3 \times 1$  vector representing the axis of rotation;  $I_{3\times 3}$  is the  $3\times 3$  identity matrix.

Note that in the actual implementation, one should be aware of the possible numerical instability due to the fact that  $\psi$  and its power in the denominator can be a quite small value (the perturbation is often associated with a small angle). Therefore, the approximation (3c) should be used when  $\psi$  (if (3a) is adopted) or  $\psi^3$  (if (3b) is adopted) is smaller than the numerical limit of a computer to avoid dividing by a value close to zero.

The inverse of the right Jacobian is then given as (see  $[1,$  Section 7.1 $]$  and  $[2]$ ):

$$
J_r(\psi)^{-1} = \frac{\psi}{2} \cot \frac{\psi}{2} I_{3 \times 3} + \left(1 - \frac{\psi}{2} \cot \frac{\psi}{2}\right) a a^T + \frac{\psi}{2} a^{\wedge}
$$
 (4a)

$$
\equiv \mathbf{I}_{3\times3} + \frac{1}{2}\,\boldsymbol{\psi}^{\wedge} + \left(\frac{1}{\psi^2} + \frac{1+\cos\psi}{2\,\psi\,\sin\psi}\right)(\boldsymbol{\psi}^{\wedge})^2 \tag{4b}
$$

$$
\approx \mathbf{I}_{3\times 3} + \frac{1}{2} \boldsymbol{\psi}^{\wedge},\tag{4c}
$$

#### 1.2 Perturbation on Lie Algebra (Middle Perturbation)

For a perturbation applied on Lie Algebra,  $\mathfrak{so}(3)$ , i.e., the tangential space of  $SO(3)$ , we let  $\phi_t$ be an angle-axis representation of a perturbation on  $\mathfrak{so}(3)$ , and we use subscript c to denote the original rotation and subscript  $d$  to mean the perturbed rotation. Thus,

$$
\exp(\theta_d^{\wedge}) = \mathbf{R}_d = \exp((\theta_c + \phi_t)^{\wedge}) \equiv \exp(\theta_c^{\wedge} + \phi_t^{\wedge})
$$
  
\n
$$
\approx \exp(\theta_c^{\wedge}) \exp((J_r(\theta_c)\phi_t)^{\wedge})
$$
  
\n
$$
= \mathbf{R}_c \exp(((J_r(\theta_c)\phi_t)^{\wedge})),
$$
\n(5)

where  $J_r(\theta_c)$  is the right jacobian evaluated at  $\theta_c$  by using (3). Notice that the perturbation is introduced in the vector space, where  $\phi_t \in \mathbb{R}^3$ .

To recover  $\boldsymbol{\theta}_d$  from  $\mathbf{R}_d$ , we have

$$
\theta_d = \ln (\mathbf{R}_d)^{\vee} = \ln (\exp (\theta_c + \phi_t)^{\wedge}))^{\vee}
$$
  
=  $\theta_c + \phi_t$  (6)

Therefore, depending on the perturbation scheme used, the form of the recovered angle-axis representation for the perturbed rotation would be slightly different.

In an optimization problem, if  $\mathbf{R}_a$  or  $\mathbf{R}_c$  represents an operating point of the rotation, and  $\phi_m$ or  $\phi_t$  represents the corresponding update, respectively. Then, if a perturbation is applied through right perturbation, the update to  $\mathbf{R}_a$  should follow (1), and one can use (2) to recover the angle-axis representation of the rotation (if a vector form is required). In contrast, if a middle perturbation is to be applied, then one would obtain a perturbation vector  $\phi_t$  from an optimization algorithm and apply the perturbation to  $\theta_c$  through (6), and the perturbed rotation matrix,  $\mathbf{R}_d$ , is obtained by applying the exponential map over  $\theta_d^{\wedge}$ .

## References

- [1] Timothy D Barfoot. State estimation for robotics. Cambridge University Press, 2017.
- [2] Christian Forster, Luca Carlone, Frank Dellaert, and Davide Scaramuzza. On-manifold preintegration for real-time visual–inertial odometry. IEEE Transactions on Robotics, 33(1):1–21, 2016.